

# Fe-Cu-REE

# U-Pb

## Re-Os

\*

1 2

1\*\*

1

1

3

1

1 2

1 2

YE XianTao<sup>1 2</sup> ZHU WeiGuang<sup>1\*\*</sup> ZHONG Hong<sup>1</sup> HE DeFeng<sup>1</sup> REN Tao<sup>3</sup> BAI ZhongJie<sup>1</sup> FAN HongPeng<sup>1 2</sup> and HU WenJun<sup>1 2</sup>

1.

1

550002

\*

2.

100049

3.

650093

1.

550002

2.

e

$^{207}\text{Pb}/^{206}\text{Pb}$

Th/U > 0.4

LA-ICP-MS U-Pb

1.75 ~ 1.88Ga 1.90 ~ 2.00Ga 2.02 ~ 2.20Ga 2.30 ~ 2.40Ga 200 3.0Ga

1750Ma

Re-Os 6 Re-Os

1690 ± 99Ma MSWD = 9.0 1685 ± 37Ma MSWD = 3.0

1.7Ga

REE

- 1.7Ga -

1.7Ga Columbia

- - U-Pb Re-Os

P595 P597.3 P611

2002

1

2

-

IOCG iron oxide-copper-gold

Greentree 2007 Zhao 2010 Zhao and Zhou 1

2011 - -

- 2004 Zhao Greentree and Li 2008

2009

2004 2005 Greentree and Li 2008 Zhao 2010 Zhao 1990 Hu 1991 -

and Zhou 2011 Zhao 2012 Chen and Zhou 2012

- 1.7Ga

- U-Pb

1687 ± 8Ma 2008 1675 ± 8Ma Greentr

2008 2009 Greentree and Li 2008 Zhao and

Zhou 2011 Chen and Zhou 2012

-

1997

1984 1990 1993 1993

1997 1999 2001

-

Fe-Cu-REE

LA-ICP-MS U-

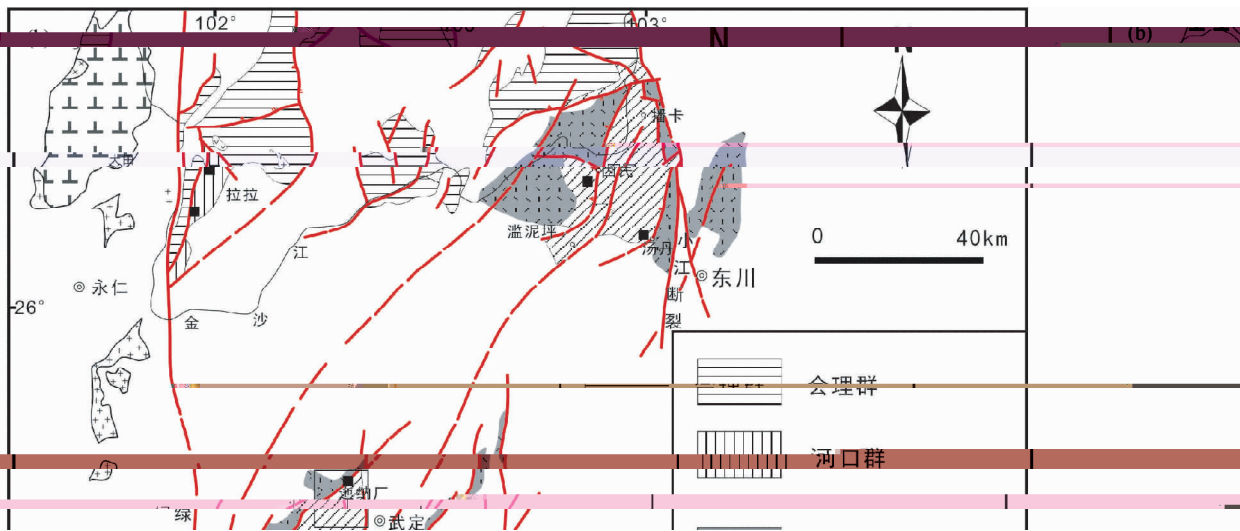
Pb

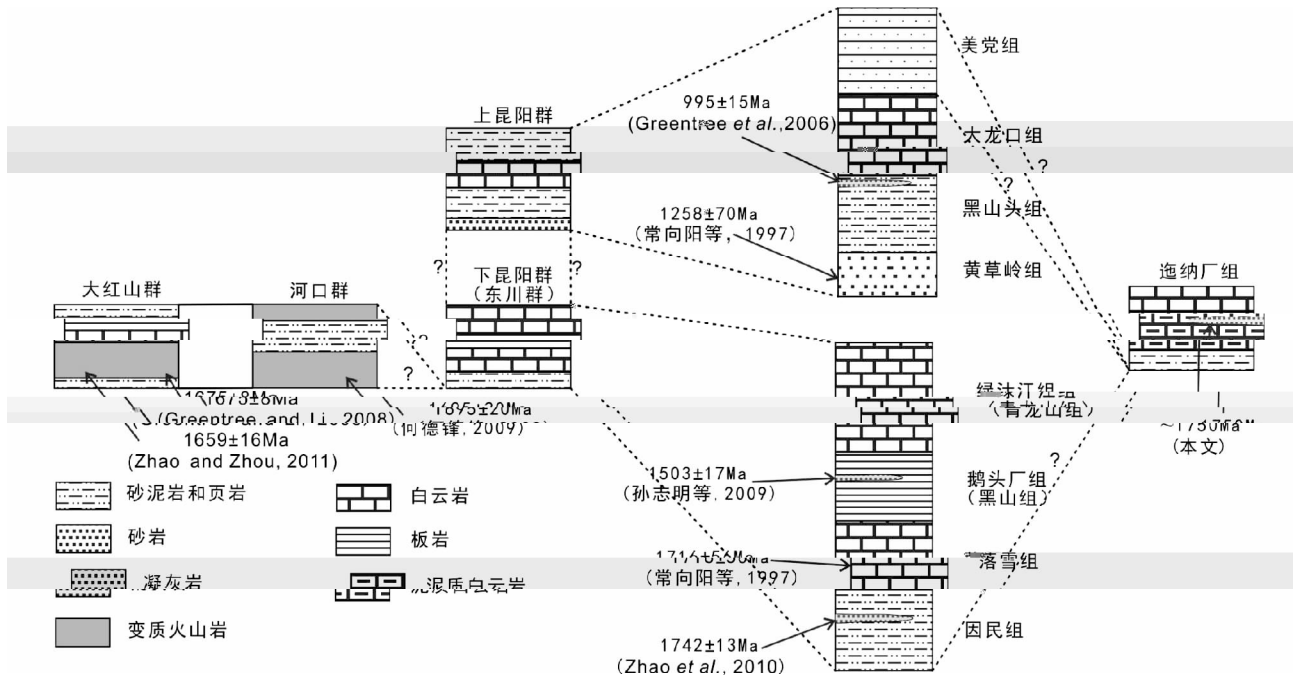
Re-Os

-

1.7Ga

Columbia Rogers and Santosh 2002 Zhao





2 Zhao and Zhou 2011

Fig.2 Stratigraphic sequences of Kuyang Group in the Kangdian region after Zhao and Zhou 2011

1032 ± 9Ma

2007

1.8 ~ 1.0Ga

400 ~ 700m

1000m 3.93 ~ 4.31m 200m

3

0.85% ~ 0.97%

41.93% ~ 44.53%

Fe-Cu-REE

2004

2004

1989

3

1cm

1mm

4a

5a b

5c d

70% 4c

5e

0.5 ~ 20cm

4b

4d

5f

8

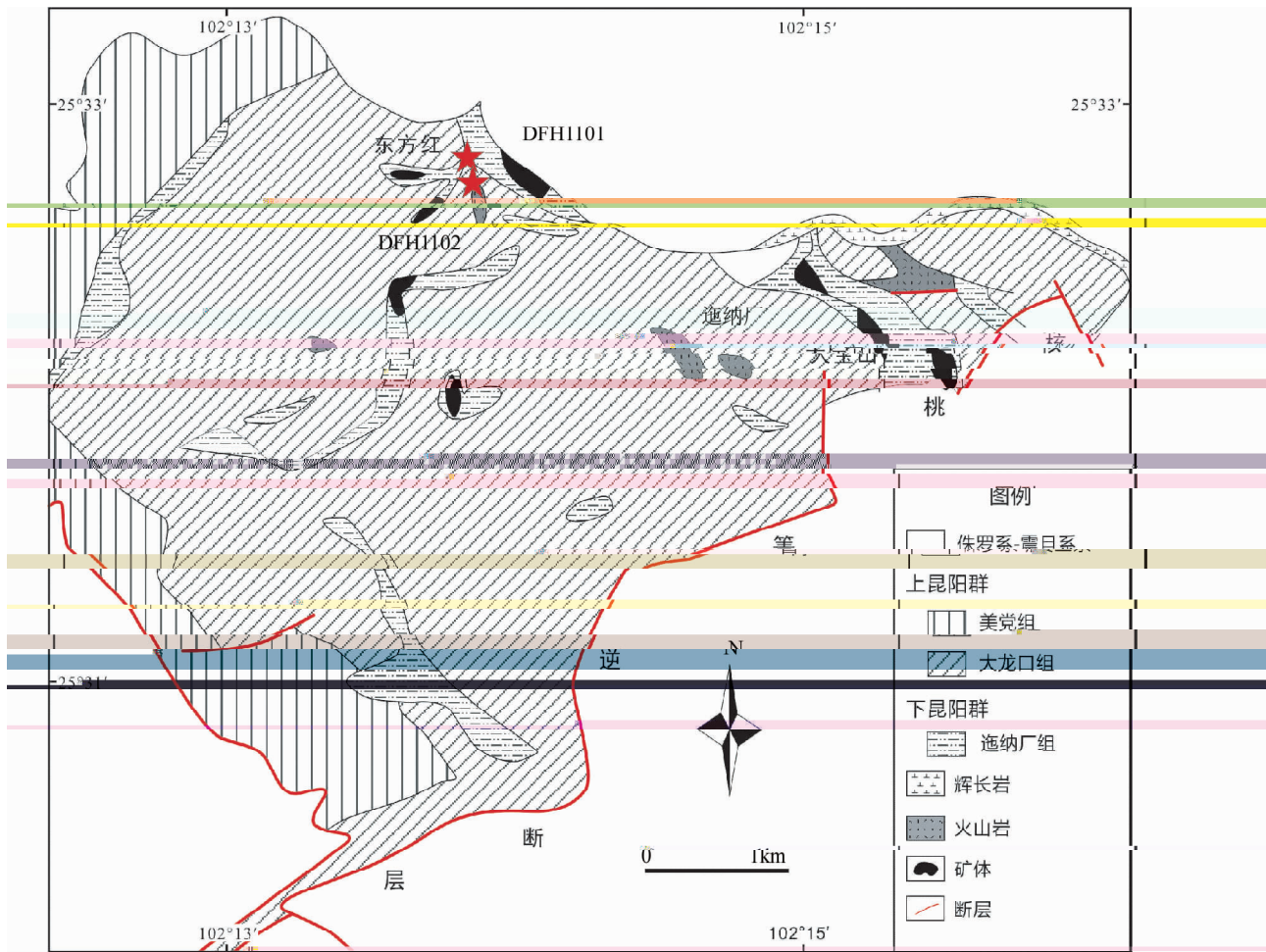
5g

3

5h

5

5i

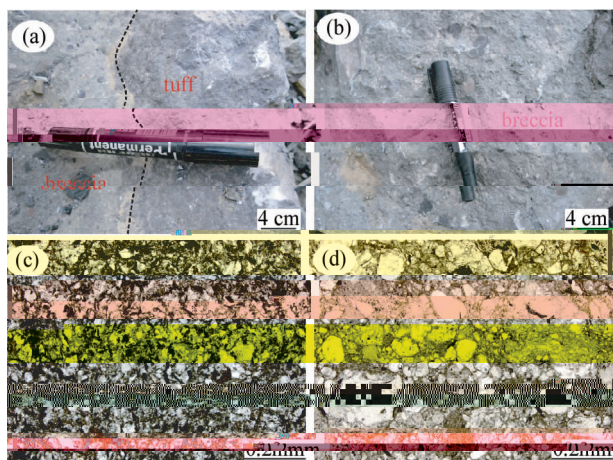


3

1990

Fig. 3 Simplified geological map of the Yinachang deposit in Wuding County Yunnan Province after Wu

1990



4

a - DFH1101 b - DFH1102

c - tuff- d - breccia-

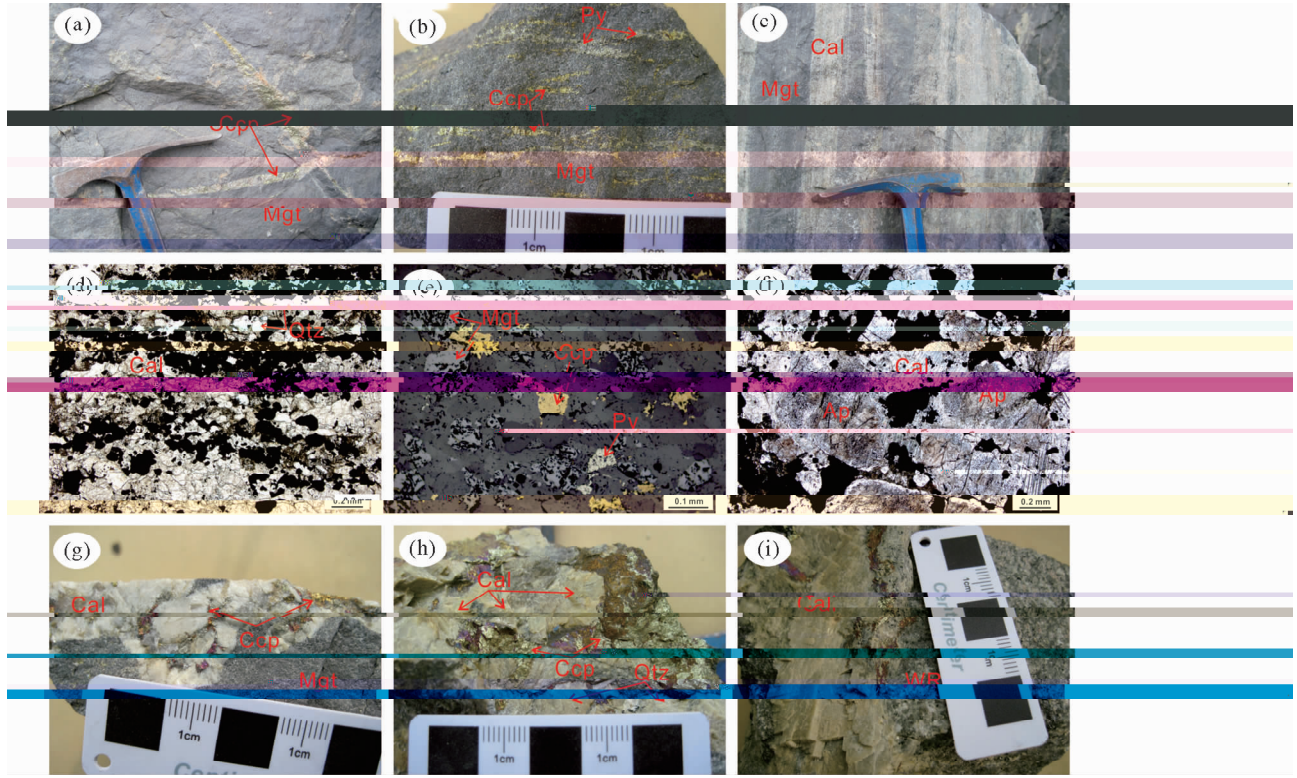
Fig. 4 Photographs and photomicrographs of the representative tuff a c and breccias b d from the Yinachang deposit

4

LA-ICP-MS U-Pb  
 DFH1101 N 25°32'53.1" E 102°13'34.3"  
 DFH1102 N 25°32'53.1" E 102°13'34.3"

CL

U-Pb

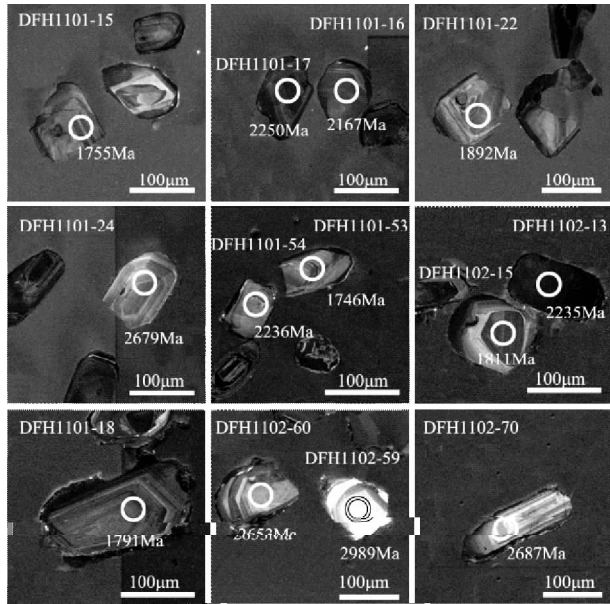


5

a b - c d - e - f - g - h -  
 i - . Cep- Cal- Py- Mgt- Ap- Qtz- WR-

Fig. 5 Photographs and photomicrographs of iron-copper ore from the Yinachang deposit

a b -vein-type ore c d -bedded ore e -disseminated ore f -apatite and calcite in the ore g -calcite in the magnetite ore h -calcite in the copper ore i -calcite in the wall-rock. Cep-chalcocopyrite Cal-calcite Py-pyrite Mgt-magnetite Ap-apatite Qtz-quartz WR-wall-rock



6

Fig. 6 Representative CL images of the detrital zircon grains for tuff and breccia from the Yinachang deposit

ICP-MS	91500
Plešovice	GJ-1
Si	NIST SRM 610
2011	Zr
Liu	Liu 2010a Hu
2010a b	ICPMSDataCal
200	40 ~ 60
ELAN DRC-e ICP-MS	99%
<sup>190</sup> Os	Re-Os
0.1g	Qi
200°C	2010
12h	<sup>185</sup> Re
Os Os 3mL	
2mol/L HCl	
AG 1-X8	Re Qi
3mL ICP-MS	2007 2010
	RSD% 3%

Table 1 LA-ICP-MS zircon U-Pb isotopic analyses of tuff and breccia in the Yinachang deposit

	$\times 10^{-6}$		Th/U	$^{207}\text{Pb}/^{206}\text{Pb}$		$^{207}\text{Pb}/^{235}\text{U}$		$^{206}\text{Pb}/^{238}\text{U}$		Ma		$1\sigma$	$1\sigma$			
	Pb	Th		$1\sigma$	$1\sigma$	$1\sigma$	$1\sigma$	$^{207}\text{Pb}/^{206}\text{Pb}$	$1\sigma$	$^{207}\text{Pb}/^{235}\text{U}$	$1\sigma$			$^{206}\text{Pb}/^{238}\text{U}$	$1\sigma$	
DFH1101																
-01	152.7	274	0.78	0.1089	0.0029	5.0129	0.1233	0.3251	0.0064	1781	48	1822	21	1815	31	99%
-02	123.9	133	0.48	0.1356	0.0014	7.0601	0.0762	0.3757	0.0023	2172	18	2119	10	2056	11	96%
-03	95.4	152	0.69	0.1186	0.0012	5.7333	0.0613	0.3492	0.0021	1935	19	1936	9	1931	10	99%
-04	80.0	128	0.82	0.1324	0.0013	7.2370	0.0759	0.3950	0.0026	2131	13	2141	9	2146	12	99%
-05	91.7	98	0.56	0.1431	0.0014	8.4020	0.0842	0.4240	0.0025	2265	18	2275	9	2279	11	99%
-06	54.7	66.0	0.60	0.1325	0.0015	7.4449	0.0840	0.4054	0.0028	2132	14	2166	10	2194	13	98%
-07	98.9	85.7	0.52	0.1521	0.0020	10.0328	0.1323	0.4764	0.0031	2369	23	2438	12	2512	13	97%
-08	221.3	119	0.17	0.1074	0.0015	4.5076	0.0628	0.3019	0.0022	1755	26	1732	12	1701	11	98%
-09	137.0	179	0.58	0.1244	0.0014	6.4374	0.0710	0.3727	0.0022	2020	-14	2037	10	2042	10	99%
-10	67.5	101	0.59	0.1096	0.0012	5.1086	0.0595	0.3363	0.0022	1794	21	1838	10	1869	11	98%
-11	88.0	69.5	0.40	0.1416	0.0014	8.7017	0.0874	0.4426	0.0027	2247	17	2307	9	2362	12	97%
-12	92.6	97	0.52	0.1409	0.0013	8.3040	0.0828	0.4251	0.0028	2239	16	2265	9	2284	12	99%
-13	53.1	98	0.63	0.1090	0.0020	4.5260	0.0816	0.2989	0.0026	1783	33	1736	15	1686	13	97%
-14	151.6	45.3	0.15	0.1359	0.0032	8.5099	0.1912	0.4487	0.0041	2176	8	2287	20	2389	18	95%
-15	48.3	78	0.66	0.1074	0.0030	4.8496	0.1339	0.3217	0.0037	1755	52	1794	23	1798	18	99%
-16	88.3	113	0.58	0.1344	0.0012	7.1352	0.0668	0.3823	0.0020	2167	15	2128	8	2087	9	98%
-17	141.2	121	0.39	0.1418	0.1418	0319.2					1		2			

Continued Table 1

	$\times 10^{-6}$		Th/U	Ma												
	Pb	Th		$^{207}\text{Pb}/^{206}\text{Pb}$	$^{207}\text{Pb}/^{235}\text{U}$	$^{206}\text{Pb}/^{238}\text{U}$	$^{207}\text{Pb}/^{206}\text{Pb}$									
-36	80.9	209	1.47	0.1200	0.0013	6.3927	0.0761	0.3834	0.0029	1967	19	2031	10	2092	14	97%
-37	87.2	64.5	0.39	0.1413	0.0014	8.6286	0.0934	0.4396	0.0030	2243	18	2300	10	2349	13	97%
-38	266.3	264	0.37	0.1105	0.0011	5.0255	0.0526	0.3267	0.0018	1809	19	1824	9	1822	9	99%
-39	101.1	93.2	0.39	0.1188	0.0014	6.0271	0.0729	0.3643	0.0026	1939	21	1980	11	2002	12	98%
-40	103.0	84.7	0.43	0.1444	0.0018	8.8538	0.1100	0.4396	0.0031	2280	21	2323	11	2349	14	98%
-41	69.0	74.6	0.55	0.1341	0.0016	7.6710	0.0938	0.4103	0.0030	2154	20	2193	11	2216	13	98%
-42	88.9	142	0.67	0.1095	0.0012	5.1544	0.0604	0.3375	0.0023	1792	20	1845	10	1875	11	98%
-43	89.6	89.3	0.43	0.1452	0.0015	7.1268	0.0931	0.3524	0.0035	2300	17	2127	12	1946	17	91%
-44	266.3	264	0.37	0.1103	0.0010	4.9246	0.0457	0.3202	0.0017	1806	16	1806	8	1791	8	99%
-45	161.9	170	0.55	0.1391	0.0013	8.2752	0.0886	0.4270	0.0031	2217	16	2262	10	2292	14	98%
-46	129.0	253	0.87	0.1203	0.0012	5.6090	0.0600	0.3350	0.0022	1961	23	1917	9	1863	10	97%
-47	211.5	374	0.85	0.1389	0.0014	7.5703	0.0909	0.3905	0.0031	2213	18	2181	11	2125	14	97%
-48	109.7	155	0.67	0.1260	0.0013	6.6323	0.0745	0.3783	0.0027	2044	18	2064	10	2068	12	99%
-49	173.7	177	0.54	0.1434	0.0013	8.7362	0.0925	0.4378	0.0031	2269	15	2311	10	2341	14	98%
-50	137.0	125	0.36	0.1169	0.0011	5.4973	0.0531	0.3382	0.0019	1910	18	1900	8	1878	9	98%
-51	215.8	177	0.51	0.1799	0.0016	12.2556	0.1307	0.4904	0.0041	2654	14	2624	10	2573	18	98%
-52	98.4	41.0	0.26	0.1785	0.0017	12.9855	0.1377	0.5232	0.0036	2639	11	2679	10	2713	15	98%
-53	48.7	68.7	0.57	0.1068	0.0013	4.8869	0.0608	0.3302	0.0027	1746	22	1800	10	1839	13	97%
-54	106.4	109	0.56	0.1406	0.0015	8.4237	0.0995	0.4313	0.0031	2236	19	2278	11	2312	14	98%
-55	134.8	120	0.39	0.1266	0.0013	6.5019	0.0767	0.3693	0.0027	2052	19	2046	10	2026	13	99%
-56	73.4	196	1.40	0.1222	0.0014	5.9134	0.0683	0.3483	0.0022	1989	20	1963	10	1926	10	98%
-57	62.0	70.0	0.59	0.1379	0.0014	7.9104	0.0866	0.4133	0.0028	2211	17	2221	10	2230	13	99%
-58	36.1	69.7	0.93	0.1208	0.0016	6.0204	0.0861	0.3598	0.0031	1969	23	1979	12	1981	15	99%
-59	82.1	263	1.58	0.1116	0.0013	5.0164	0.0616	0.3236	0.0023	1828	21	1822	10	1807	11	99%
-60	187.0	197	0.56	0.1432	0.0015	8.3718	0.0911	0.4207	0.0027	2266	18	2272	10	2264	12	99%
-61	49.4	77.2	0.93	0.1454	0.0019	8.8411	0.1230	0.4378	0.0035	2294	23	2322	13	2341	16	99%
-62	123.4	92.1	0.37	0.1429	0.0015	8.1120	0.0905	0.4081	0.0025	2263	19	2244	10	2206	12	98%
-63	215.1	194	0.45	0.1451	0.0014	8.2793	0.0852	0.4102	0.0023	2289	17	2262	9	2216	10	97%
-64	133.9	124	0.42	0.1377	0.0014	7.0855	0.0792	0.3696	0.0026	2198	18	2122	10	2028	12	95%
-65	160.0	132	0.40	0.1434	0.0014	7.9348	0.0791	0.3978	0.0024	2269	17	2224	9	2159	11	97%
-66	79.1	70.6	0.41	0.1253	0.0014	6.7131	0.0808	0.3852	0.0028	2035	20	2074	11	2101	13	98%
-67	62.0	61.8	0.57	0.1456	0.0017	9.2008	0.1131	0.4555	0.0035	2295	20	2358	11	2420	16	97%
-68	63.2	77.5	0.49	0.1106	0.0014	5.2508	0.0704	0.3418	0.0027	1810	23	1861	11	1895	13	98%
-69	123.9	94.3	0.40	0.1459	0.0017	8.7938	0.1075	0.4335	0.0030	2298	19	2317	11	2321	13	99%
-70	151.1	340	1.13	0.1213	0.0013	6.1160	0.0688	0.3626	0.0024	1976	14	1993	10	1994	11	99%
-71	63.0	75.0	0.64	0.1443	0.0016	8.6918	0.0966	0.4329	0.0027	2279	19	2306	10	2319	12	99%



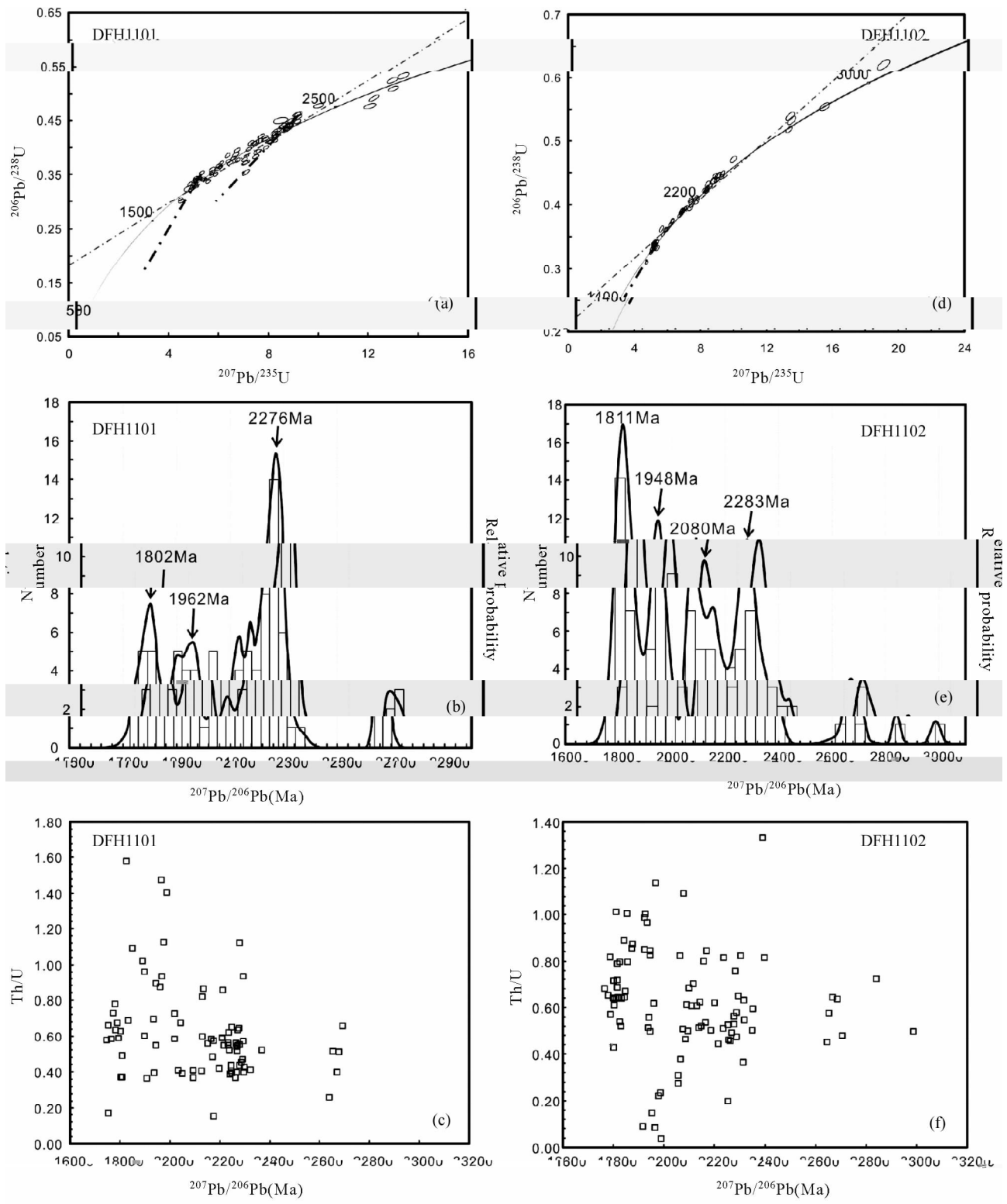
Continued Table 1

	$\times 10^{-6}$		Th/U	Ma											
	Pb	Th		$^{207}\text{Pb}/^{206}\text{Pb}$	$^{207}\text{Pb}/^{235}\text{U}$	$^{207}\text{Pb}/^{206}\text{Pb}$	$^{207}\text{Pb}/^{235}\text{U}$								
-72	136.9	136	0.66	0.0018	13.0323	0.1292	0.5076	0.0030	2694	16	2682	9	2646	13	98%
-73	122.1	150	0.65	0.0014	8.3021	0.0890	0.4200	0.0027	2250	50	2265	10	2260	12	99%
-74	144.7	227	0.86	0.0013	7.7595	0.0846	0.4192	0.0030	2135	18	2204	10	2257	13	97%
-75	156.1	143	0.41	0.0013	6.7816	0.0713	0.3749	0.0023	2094	23	2083	9	2052	11	98%
-76	118.4	169	0.58	0.0013	5.0668	0.0618	0.3367	0.0025	1766	21	1831	10	1871	12	97%
-77	88.2	103	0.62	0.0015	8.5921	0.1031	0.4386	0.0035	2237	19	2296	11	2344	16	97%
-78	123.2	151	0.55	0.0012	6.1333	0.0680	0.3691	0.0027	1946	18	1995	10	2025	13	98%
-79	64.8	96.5	0.72	0.0013	6.7847	0.0806	0.3925	0.0030	2020	-14	2084	11	2134	14	97%
-80	63.0	109	0.73	0.0012	5.1333	0.0626	0.3408	0.0026	1773	20	1842	10	1890	12	97%
-81	143.8	111	0.37	0.0012	7.3295	0.0815	0.4065	0.0031	2094	17	2152	10	2199	14	97%
-82	64.1	65.3	0.55	0.0016	8.8574	0.1082	0.4419	0.0035	2280	20	2323	11	2359	16	98%
-83	133.1	168	0.59	0.0014	7.1239	0.0875	0.3709	0.0030	2211	17	2127	11	2034	14	95%
-84	79.6	109	0.60	0.0014	5.7745	0.0709	0.3580	0.0025	1898	22	1943	11	1973	12	98%
DFH102															
-01	87.6	164	0.82	0.0012	4.9917	0.0618	0.3287	0.0025	1787	22	1818	10	1832	12	99%
-02	24.28	34.6	0.61	0.0016	5.2812	0.0836	0.3466	0.0035	1806	21	1866	14	1918	17	97%
-03	36.8	62	0.68	0.0016	4.8210	0.0728	0.3235	0.0029	1767	27	1789	13	1807	14	98%
-04	213.4	230	0.49	0.0012	7.1364	0.0634	0.3575	0.0017	2270	15	2129	8	1971	8	92%
-05	113.9	114	0.52	0.0012	7.5570	0.0714	0.4069	0.0024	2148	17	2180	8	2201	11	99%
-06	62.8	91.4	0.82	0.0016	8.9171	0.1226	0.4145	0.0041	2399	18	2330	13	2235	19	95%
-07	53.3	122	1.01	0.0013	4.8264	0.0546	0.3159	0.0018	1811	16	1790	10	1770	9	98%
-08	74.5	104	0.68	0.0015	6.7038	0.0784	0.3709	0.0025	2102	20	2073	10	2034	12	98%
-09	123.5	154	0.62	0.0014	6.9575	0.0832	0.3754	0.0031	2143	19	2106	11	2055	14	97%
-10	252.0	284	0.63	0.0018	8.1843	0.0999	0.3968	0.0026	2317	21	2252	11	2154	12	95%
-11	95.2	86.7	0.64	0.0017	13.2204	0.1292	0.5231	0.0032	2668	15	2696	9	2712	14	99%
-12	200.3	67.7	0.15	0.0012	6.0441	0.0620	0.3623	0.0020	1954	13	1982	9	1993	9	99%
-13	114.0	107	0.51	0.0013	8.3927	0.0873	0.4291	0.0030	2235	16	2274	9	2302	13	98%
-14	85.6	91.3	0.50	0.0021	6.0186	0.0983	0.3624	0.0029	1946	38	1979	14	1994	14	99%
-15	49.0	76.3	0.64	0.0014	5.0646	0.0700	0.3313	0.0029	1811	18	1830	12	1845	14	99%
-16	75.7	131	0.84	0.0014	5.9654	0.0721	0.3601	0.0025	1946	21	1971	11	1983	12	99%
-17	33.53	22.3	0.45	0.0022	13.4050	0.1688	0.5381	0.0045	2647	53	2709	12	2775	19	97%
-18	49.4	68.7	0.57	0.0012	4.9766	0.0554	0.3283	0.0023	1791	20	1815	9	1830	11	99%
-19	61.6	61.1	0.50	0.0013	7.6532	0.0773	0.4029	0.0026	2187	17	2191	9	2182	12	99%
-20	79.6	92.6	0.51	0.0012	5.8956	0.0590	0.3577	0.0022	1939	23	1961	9	1971	10	99%
-21	49.6	82.1	0.82	0.0013	6.7275	0.0734	0.3794	0.0026	2065	13	2076	10	2073	12	99%
-22	63.0	62.8	0.53	0.0015	8.5432	0.0972	0.4267	0.0029	2280	19	2291	10	2291	13	99%



Continued Table 1

	$\times 10^{-6}$		Th/U	Ma											
	Pb	Th		$^{207}\text{Pb}/^{206}\text{Pb}$	$^{206}\text{Pb}/^{238}\text{U}$	$^{207}\text{Pb}/^{206}\text{Pb}$	$^{207}\text{Pb}/^{235}\text{U}$	$^{206}\text{Pb}/^{238}\text{U}$							
	U	$1\sigma$		$1\sigma$	$1\sigma$	$1\sigma$	$1\sigma$	$1\sigma$							
-59	31.92	19.8	0.50	0.0026	18.8909	0.2486	0.6217	0.0055	2989	19	3036	13	3117	22	97%
-60	55.9	47.1	0.57	0.0020	13.4778	0.1675	0.5401	0.0042	2653	18	2714	12	2784	17	97%
-61	26.04	43.5	0.71	0.0016	5.1550	0.0768	0.3391	0.0027	1802	26	1845	13	1882	13	98%
-62	112.5	59.0	0.22	0.0014	6.3109	0.0740	0.3741	0.0024	1981	53	2020	10	2048	11	98%
-63	47.2	55.3	0.65	0.0019	8.8067	0.1194	0.4369	0.0033	2295	22	2318	12	2337	15	99%
-64	76.7	119	0.64	0.0012	5.1465	0.0640	0.3371	0.0025	1799	16	1844	11	1873	12	98%
-65	44.3	70.9	0.67	0.0014	5.2148	0.0658	0.3337	0.0023	1847	23	1855	11	1856	11	99%
-66	29.14	52.5	0.80	0.0016	5.2541	0.0746	0.3412	0.0024	1825	26	1861	12	1892	12	98%
-67	63.2	128	0.99	0.0014	5.8883	0.0706	0.3604	0.0025	1925	20	1960	10	1984	12	98%
-68	51.6	65.7	0.52	0.0014	5.2242	0.0701	0.3365	0.0025	1832	23	1857	11	1870	12	99%
-69	86.1	82.9	0.72	0.0024	15.5602	0.1927	0.5550	0.0039	2842	14	2850	12	2846	16	99%
-70	46.0	42.0	0.64	0.0022	13.5549	0.1696	0.5334	0.0044	2687	20	2719	12	2756	19	98%
-71	59.9	85.4	0.81	0.0016	8.4530	0.1001	0.4327	0.0031	2237	20	2281	11	2318	14	98%
-72	54.9	92.8	0.72	0.0013	5.1143	0.0623	0.3320	0.0023	1817	21	1838	10	1848	11	99%
-73	19.44	20.6	0.58	0.0021	8.8198	0.1403	0.4382	0.0042	2289	24	2320	15	2343	19	99%
-74	43.9	62.1	0.64	0.0014	5.6604	0.0775	0.3616	0.0032	1847	18	1925	12	1990	15	96%
-75	52.0	69.6	0.70	0.0015	7.4376	0.0966	0.4073	0.0032	2117	21	2166	12	2202	15	98%
-76	51.9	81.3	0.64	0.0014	5.0472	0.0683	0.3250	0.0023	1833	18	1827	11	1814	11	99%
-77	135.6	54.7	0.20	0.0016	8.3715	0.0974	0.4228	0.0028	2254	20	2272	11	2273	13	99%
-78	48.6	53.1	0.54	0.0018	7.4327	0.1073	0.3946	0.0031	2165	23	2165	13	2144	14	99%
-79	79.1	93.5	0.61	0.0015	7.4413	0.0910	0.4038	0.0029	2131	20	2166	11	2187	13	99%
-80	105.5	131	0.56	0.0012	5.9883	0.0654	0.3611	0.0024	1943	19	1974	10	1987	11	99%
-81	173.4	174	0.54	0.0014	9.0175	0.0919	0.4386	0.0028	2318	21	2340	9	2344	12	99%
-82	150.7	227	0.80	0.0013	7.4881	0.0761	0.3989	0.0024	2159	17	2172	9	2164	11	99%
-83	160.0	213	0.62	0.0012	6.0871	0.0616	0.3630	0.0020	1961	23	1988	9	1996	10	99%
-84	54.2	84.6	0.64	0.0014	5.0491	0.0645	0.3255	0.0022	1820	22	1828	11	1816	11	99%
-85	30.4	56.5	0.80	0.0018	5.3533	0.0895	0.3403	0.0033	1858	29	1877	14	1888	16	99%
-86	111.2	68.5	0.27	0.0014	6.7727	0.0780	0.3827	0.0025	2057	18	2082	10	2089	12	99%
-87	80.5	84.9	0.59	0.0016	9.3012	0.1041	0.4435	0.0029	2353	19	2368	10	2366	13	99%
-88	44.90	36.6	0.38	0.0015	6.9153	0.0855	0.3895	0.0028	2066	16	2101	11	2121	13	99%
-89	86.3	134	0.84	0.0014	7.7422	0.0859	0.4104	0.0029	2170	17	2202	10	2217	13	99%
-90	149.3	102	0.31	0.0013	6.8407	0.0719	0.3864	0.0023	2058	18	2091	9	2106	11	99%
-91	58.7	53.0	0.47	0.0016	8.6416	0.1050	0.4291	0.0031	2287	19	2301	11	2302	14	99%
-92	39.6	60.6	0.63	0.0015	5.1442	0.0720	0.3354	0.0024	1806	24	1843	12	1865	12	98%
-93	61.9	62.3	0.53	0.0018	8.3089	0.1079	0.4230	0.0029	2256	50	2265	12	2274	13	99%



7 U-Pb  $^{207}\text{Pb}/^{206}\text{Pb}$  Th/U- $^{207}\text{Pb}/^{206}\text{Pb}$   
 Fig. 7 Plot of U-Pb concordant curve  $^{207}\text{Pb}/^{206}\text{Pb}$  age frequency and Th/U- $^{207}\text{Pb}/^{206}\text{Pb}$  age diagram of the det d 0 0

Table 2 Re-Os isotope compositions for chalcopyrite from the Yinachang deposit

	$^{187}\text{Re}$ $\times 10^{-9}$	$1\sigma$	$^{187}\text{Os}$ $\times 10^{-9}$	$1\sigma$	Re $\times 10^{-9}$	$1\sigma$	Os $\times 10^{-9}$	$1\sigma$	Ma	$1\sigma$
YNC1006	562.306	16.269	16.881	0.314	898.253	25.989	0.023	0.006	1732	23
10YNC-40	161.659	2.145	4.455	0.061	258.242	3.426	0.017	0.001	1638	22
YNC1010	4.615	0.108	0.118	0.003	7.373	0.172	0.003	0.000	1719	20
10YNC-32	12.859	0.300	0.366	0.004	20.541	0.480	0.004	0.000	1690	20
10YNC-41	246.010	30.390	6.836	0.079	392.988	48.547	0.005	0.001	1651	19
YNC1112	4.388	0.149	0.073	0.005	7.010	0.239	0.002	0.000	1687	19

5

8a

5.1 U-Pb

LA-ICP-MS

U-Pb

1 6

CL

7

U-Pb

 $^{207}\text{Pb}/$  $^{206}\text{Pb}$ Th/U- $^{207}\text{Pb}/^{206}\text{Pb}$ 

DFH1101

2000

84

95%

 $^{207}\text{Pb}/^{206}\text{Pb}$  $1746 \pm 22\text{Ma}$  $^{207}\text{Pb}/^{206}\text{Pb}$  $2694 \pm 16\text{Ma}$ 

5

2500Ma

1.75 ~ 1.85Ga

1.90 ~ 2.00Ga 2.20 ~ 2.35Ga

 $^{207}\text{Pb}/^{206}\text{Pb}$  $1796 \pm 15\text{Ma}$  n

= 16 MSWD = 1.5

 $2262 \pm 12\text{Ma}$  n = 34 MSWD = 3.5

1800Ma

1960Ma

2270Ma

7b

CL

6 Th/U

0.1

0.4 ~ 1.0

7c

DFH1102

2500

93

95%

 $^{207}\text{Pb}/^{206}\text{Pb}$  $1767 \pm 27\text{Ma}$  $^{207}\text{Pb}/^{206}\text{Pb}$  $2989 \pm 19\text{Ma}$ 

7

2500Ma

1.75

~ 1.88Ga 1.90 ~ 2.00Ga 2.02 ~ 2.20Ga 2.30 ~ 2.40Ga

 $^{207}\text{Pb}/^{206}\text{Pb}$  $1796 \pm 9\text{Ma}$  n = 19 MSWD = 0.71

Th/U

1800Ma

1950Ma

2080Ma

2280Ma

7e

CL

06592608 TD (Y) 0659265935Lq (Y) 200494506 0 TD (a) Tj 92.123506 0 TD (u) Tj 0.78022 0 TD ( ) Tj /F3 1 Tf 0 Tr 8.830188 0 0 8

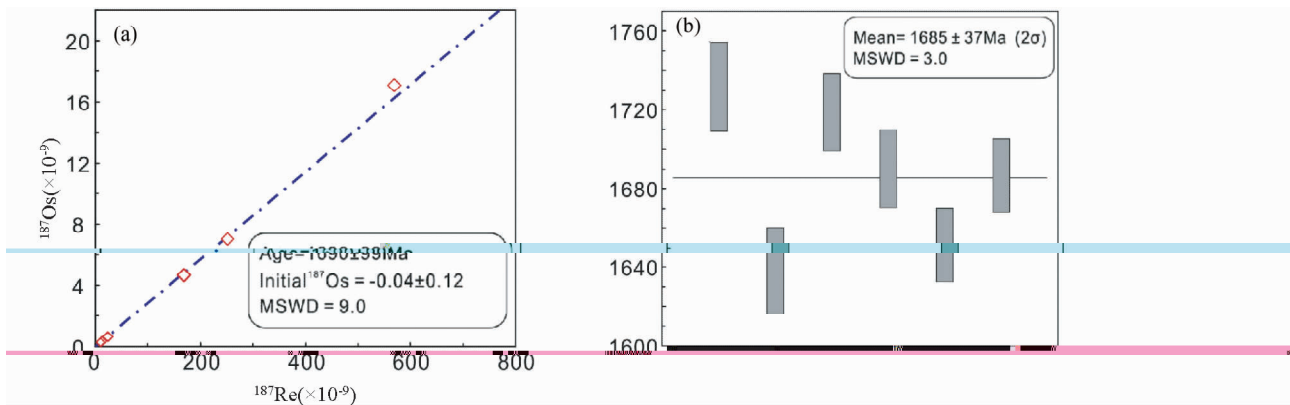
~ 1.0

7f

U-Pb

Table 3 Rare earth elements REE contents  $\times 10^{-6}$  of ores and wall-rock from the Yinachang deposit

	La	Ce	Pr	Nd	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb	Lu	$\Sigma$ REE	$\delta$ Eu	$\delta$ Ce	La/Yb <sub>N</sub>	La/Sm <sub>N</sub>	Gd/Yb <sub>N</sub>	LREE/ HREE
10YNC-31	670	1050	108	340	54.8	29	37.9	5.38	27.4	4.46	10	1.36	6.2	0.5	2345	1.95	0.94	72.86	7.69	4.93	24.16
10YNC-41	584	983	101	320	53.1	30.9	38.9	6.07	32.1	5.92	14.2	2.04	9.7	0.94	2182	2.08	0.97	40.59	6.92	3.24	18.86
DFH1111	264	421	41.1	128.5	19.5	11.8	12.5	1.63	8.9	1.61	4.4	0.87	5.3	0.57	922	2.31	0.97	33.58	8.52	1.90	24.76
DFH1112	609	961	97.9	319	52.1	44.4	42.1	6	31.2	6.02	14.3	1.78	8.9	0.73	2194	2.90	0.95	46.13	7.35	3.82	18.76
YNC1003	186	340	47.2	179	38.1	26.4	36.8	6.09	35	6.95	17.9	2.12	11.3	1.13	934	2.16	0.87	11.10	3.07	2.63	6.96
YNC1004	31.2	53.1	5.05	17.1	2.6	3.09	2.08	0.23	0.975	0.154	0.404	0.0453	0.284	0.033	116	4.06	1.02	74.07	7.55	5.92	26.63
YNC1011	144	228	21.4	74.5	14.6	19.8	15.9	2.88	16.7	3.74	9.87	1.33	6.93	0.783	805	3.97	0.99	14.01	6.20	1.85	8.64
YNC1015	217	335	29.9	102	18.3	24.1	20.9	3.86	22.8	5.38	13.3	1.73	9.54	1.08	560	3.77	1.00	15.34	7.46	1.78	9.23
YNC1006	129	279	31.6	124	27.6	10.3	29.5	5.38	31.9	7.09	18.5	2.34	12	1.18	709	1.10	1.05	7.25	2.94	1.98	5.58
YNC1007	125	249	26.8	99.7	19.5	7.6	19.3	2.98	15.2	2.96	7.24	0.853	4.58	0.477	581	1.20	1.04	18.40	4.03	3.41	9.84
YNC1008	169	322	41.2	158	25.3	8.55	20.4	3.1	14.9	3.31	8.54	1.17	6.48	0.747	783	1.15	0.93	17.58	4.20	2.55	12.35
YNC1009	2180	4320	525	1890	374	125	320	52.8	320	68.3	159.5	20.7	88.2	8.2	10452	1.11	0.97	16.66	3.67	2.93	9.07
YNC1010	251	640	90.9	370	93.7	45.8	93.9	17.4	104	21.4	51.6	5.89	26.5	2.45	6223	1.49	1.02	6.39	1.69	2.86	4.61
YNC1012	382	978	120	572	130	60.7	147	26.9	163	36.3	88.4	10.3	46.6	4.36	10736	1.34	1.10	5.53	1.85	2.54	4.29
YNC1013	356	1111	121	496	102	43.3	97.9	17.7	98.6	20.1	47.3	5.31	23.8	2.28	4802	1.32	1.29	10.08	2.20	3.32	7.12
YNC1014	1060	2423	279	1320	271	87.6	268	43.8	235	48.2	112	12.7	57.9	5.17	2766	0.99	1.07	12.34	2.46	3.73	6.95
10YNC-30	2350	4630	558	1970	361	126	274	40.6	223	43.3	94.1	12.3	49.6	4.35	2542	1.22	0.97	31.94	4.09	4.46	13.48
10YNC-32	1035	2040	24	90	2354	07		3				2	5	8	1	3	2	2	5		3



8 Re-Os a b  
 Fig. 8 Isochrone age diagram a and weighted average of model age b of Re-Os isotope for chalcopyrite of the Yinachang deposit

Σ REE = 207

<p>× 10<sup>-6</sup> ~ 270 × 10<sup>-6</sup></p> <p>La/Yb<sub>N</sub> 14.1 ~ 23.9</p> <p>~ 7.1 LREE/HREE 11.2 ~ 16.9</p> <p>= 2.31 ~ 2.50</p>	<p>La/Sm<sub>N</sub> 4.8</p> <p>δEu</p> <p>δCe = 1.1</p> <p>3 9c</p>	<p>1780Ma</p> <p>13Ma Zhao 2010</p> <p>U-Pb 1690 ± 32Ma Zhao 2010</p> <p>1.7Ga</p> <p>2012</p> <p>2008 Greentree and Li 2008 Zhao and Zhou</p> <p>2011</p> <p>± 20Ma 2009</p> <p>1710 ± 8Ma U-Pb 2011</p>
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6 1742 ±

6.1 1711 ± 4Ma

1954 1.7Ga

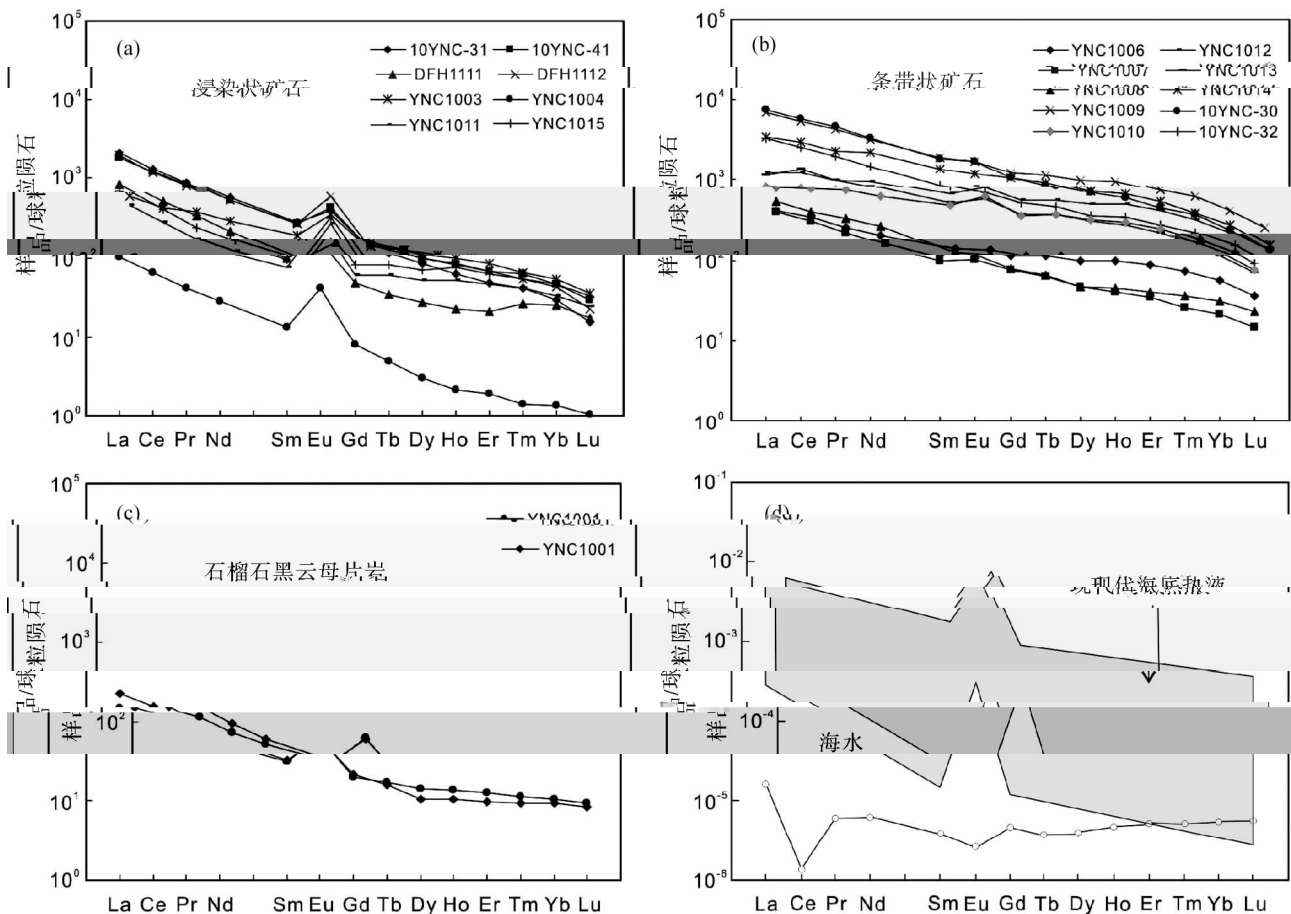
1990

<p>1993</p> <p>and Li 2008 Zhao 2010</p> <p>DFH1101</p> <p>22Ma</p> <p>68.7 × 10<sup>-6</sup></p> <p>DFH1102</p> <p>27Ma U 91 × 10<sup>-6</sup> Th 62 × 10<sup>-6</sup></p> <p>0.68</p> <p>1750Ma</p>	<p>1995</p> <p>Zhang 2006 Greentree</p> <p>LA-ICP-MS U-Pb</p> <p>1746 ±</p> <p>U 120 × 10<sup>-6</sup> Th</p> <p>Th/U 0.57</p> <p><sup>207</sup>Pb/<sup>206</sup>Pb 1767 ±</p> <p>Th/U</p> <p>1750Ma</p>	<p>~ 2280Ma 2.5Ga</p> <p>~ 1800Ma ~ 1950Ma ~ 2080Ma</p>
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6.2 Fe-Cu-REE







9 a b c  
d Craddock 2010 Elderfield and Greaves 1982

Boynton 1984

Fig. 9 Chondrite-normalized REE patterns for disseminated ores a banded ores b and garnet biotite schist c of the Yinachang deposit

REE patterns for submarine hydrothermal fluids after Craddock 2010 REE pattern for seawater after Elderfield and Greaves 1982 chondrite-normalizing values after Boynton 1984

IOCG

7

1.7Ga

1  
LA-ICP-MS U-Pb

1750Ma

1.7Ga Columbia  
Rogers and Santosh 2002

2 Fe-Cu-REE Re-Os  
1690 ± 99Ma

1.7Ga

Zhao 2002

3

Columbia  
2011 Wang 2012 Yu 2012  
1.7Ga

Zhao and Zhou

Fe-Cu

U-Pb

Re-Os

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